J. D. LEE ENGINEERING LIMITED

CONSULTING ENGINEERS

P. O. BOX 1267

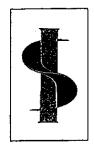
155 DIVISION STREET

KINGSTON, ONTARIO K7L 4Y8

TOWN OF NAPANEE

WATER POLLUTION CONTROL PLANT

STAGE 2 CONTRACT. SOIL INVESTIGATION



SITE INVESTIGATION SERVICES

677 CROWN DRIVE PETERBORQUIGH, ONT. PHONE 743-6850

October 5, 1977

J.D. LEE ENGINEERING LIMITED Consulting Engineers P. O. Box 1267 155 Division Street KINGSTON, Ontario K7L 4Y8

Attention: Mr. J. D. Lee, P. Eng.

Re: Town of Napanee, Water Pollution Control Plant Stage 2 Contract. Soil Investigation

Dear Sir:

We have completed an evaluation of soil conditions for the above project.

This letter describes soil and groundwater conditions encountered in seven boreholes and discusses requirements for the design and construction of foundations for the proposed structures.

Borehole locations, as shown on Figure 1, were generally as shown on your drawing 1209C, sent to us on September 21, 1977. However, two of the boreholes had to be shifted to avoid trees and the existing sludge drying beds.

SOIL CONDITIONS

<u>Soil Profile</u> - Soil profile and test data at the boreholes are summarized on Figures 3 to 8 and a general soil profile is shown on Figure 2.

Native soils consist of 18 to 25 feet of layered silty clay underlain by 2 to 5 feet of layered sandy silt to silty fine sand. At holes 4, 5, 6 and 7 the silty sand - sandy silt stratum is underlain by bedrock while at borehole 1 there is a thin

layer of stony clayey silty sand till separating the bedrock and sandy silt layer. Boreholes 2 and 3 were terminated in the silty sand stratum. The native soils have been covered by 4 to 6 feet of gravel fill and rubble fill near holes 1, 2 and 3.

The bottom of the silty clay stratum and the bedrock surface slope downward from north to south. In this regard the bedrock surface is near elevation 237 feet at boreholes 4 and 6 (north end) and below elevation 227 feet at boreholes 2 and 3 (south end). The silty clay - silty sand interface is near elevation 240 feet at holes 4 and 6 and below elevation 230 feet at borehole 3.

<u>Silty Clay</u> - The silty clay stratum consists primarily of layered to varved silty clay soils. However there are occasional clayey silt lenses and occasional thin (1/8 inch or less) partings of silty fine sand.

The upper several feet of clay is very stiff as indicated by standard penetration resistances of 12 to 24 blows per foot. The consistency decreases with depth. Vane shear strengths of 2000 to 2250 and standard penetration resistances of 4 to 7 were measured in the lower clay soils at boreholes 2 and 3. These soils are classified as stiff to very stiff.

<u>Sand - Silt - The soil stratum below the silty clay is coarsest near boreholes 2 and</u>
3 and generally becomes finer towards the north. However there are thin sandier seams in some of the northerly areas. The particle size range shown on Figure 10 is typical for the coarser soils in this stratum. Particle sized on Figure 11 are typical of the predominent non plastic sandy coarse silt found at the northerly end of the site.

There are some seams of silty clay in the sand - silt stratum. The frequency of the clay seams increases in a northerly direction.

 $\underline{\mathtt{Bedrock}}$ - Bedrock levels were inferred from depths where the augers met refusal. This refusal depth normally coincides with the bedrock surface.

Bedrock in the Napanee area consists of bedded limestone. The bedrock can be assumed to be sound for the purposes of this report.

GROUNDWATER CONDITIONS

Water level measurements were taken in the open boreholes after drilling. In addition piezometers were installed in the silty sand to sandy silt stratum (near the bedrock surface). Bentonite seals were placed in the silty clay stratum to ensure that hydrostatic pressures in the silty sand - sandy silt stratum are not relieved near the piezometer tips.

A slight artesian water pressure condition existed in the stily sand - sandy silt stratum on October 4, 1977. In this regard piezometric water levels in the piezometers near boreholes 5 and 7 were 2.5 to 3.5 feet higher than the groundwater levels measured in the adjacent open boreholes. The open borehole water levels reflect the groundwater level conditions in the upper clay soils.

Seasonal fluctuations of the artesian water levels will occur. Some idea of possible ranges can be obtained by monitoring the water level fluctuations in the piezometers until the plant is built. Monthly or bi-monthly readings are recommended.

DESIGN AND CONSTRUCTION CONSIDERATIONS

General - All of the inorganic native soils are competent to support the relatively light structure loads (less than 2000 pounds per square foot). Settlements should be small provided that the subsoils are not disturbed during construction. Careful, planned excavation procedures are required to ensure against subsoil disturbance. Potential excavation problems are discussed in the following section.

Excavations - The silty clay stratum acts as an impervious blanket and probably will prevent relief of water pressures in the underlying silty sand - sandy silt stratum. In deeper excavations, where the base is within several feet of the silty sand - sandy silt stratum, the artesian water pressures can cause the base of the excavation to fail. Characteristically the failure consists of a heave of the unexcavated clay above the silty sand - sandy silt stratum or a base heave accompanied by a slump of the surrounding excavation slopes. Once the silty clay heaves, the silty sand and sandy silt will boil through cracks and fissures.

The stability of the base can be ensured by keeping hydrostatic water levels in the silty sand - sandy silt stratum close to or below the base of the excavation. Such a decline might occur naturally during dry periods. We expect, however, that vacuum wellpoints or some alternative dewatering procedure will be required to control water levels.

The above described problem condition is most severe near boreholes 1, 4, 5 and 6 where the structure base is close to the silty sand - sandy silt stratum. This is illustrated on Figure 2. The problem is less severe near holes 2, 3 and 7 where the excavation depth is less and the clay layer extends to a deeper elevation. In actual fact we expect that the shallower excavations near holes 2, 3 and 7 could be completed without dewatering if artesian water levels during construction are a few feet lower than those measured on October 4, 1977.

Dewatering requirements for the artesian aquifer could be decreased by shifting the structure to the deeper clay zones near the river. However, problems with water in the upper fill zones could occur in this area.

<u>Uplift on Structures</u> - Artesian pressures in the silty sand - sandy silt stratum should be considered when computing the uplift of deeper structure areas near holes 1, 4, 5 and 6. In these areas it is conceivable that the artesian pressures could lift the overlying soil and the empty structures. If there is any concern about uplift resistance

we would suggest that some form of underdrainage system be provided to relieve partially the artesian pressures. An underdrainage system could consist of two 4 to 5 foot trenches below the northerly part of the structure. These narrow trenches would intersect the silty sand - sandy silt soils and permit relief of water pressure. The trenches should be backfilled with concrete sand. The concrete sand will act as a filter that will prevent migration of the fine sands and silts.

<u>Working Surface</u> - If 3/4 inch stone is used for a working surface it should be underlain by at least 8 inches of concrete sand or granular B close to concrete sand limits. The sand will prevent material from silt or fine sand seams from migrating into the crushed stone.

I trust that the information in this letter - report is adequate for your requirements. However, should you have any queries or should you wish us to review dewatering and uplift designs, please do not hesitate to contact us.

Yours very truly,

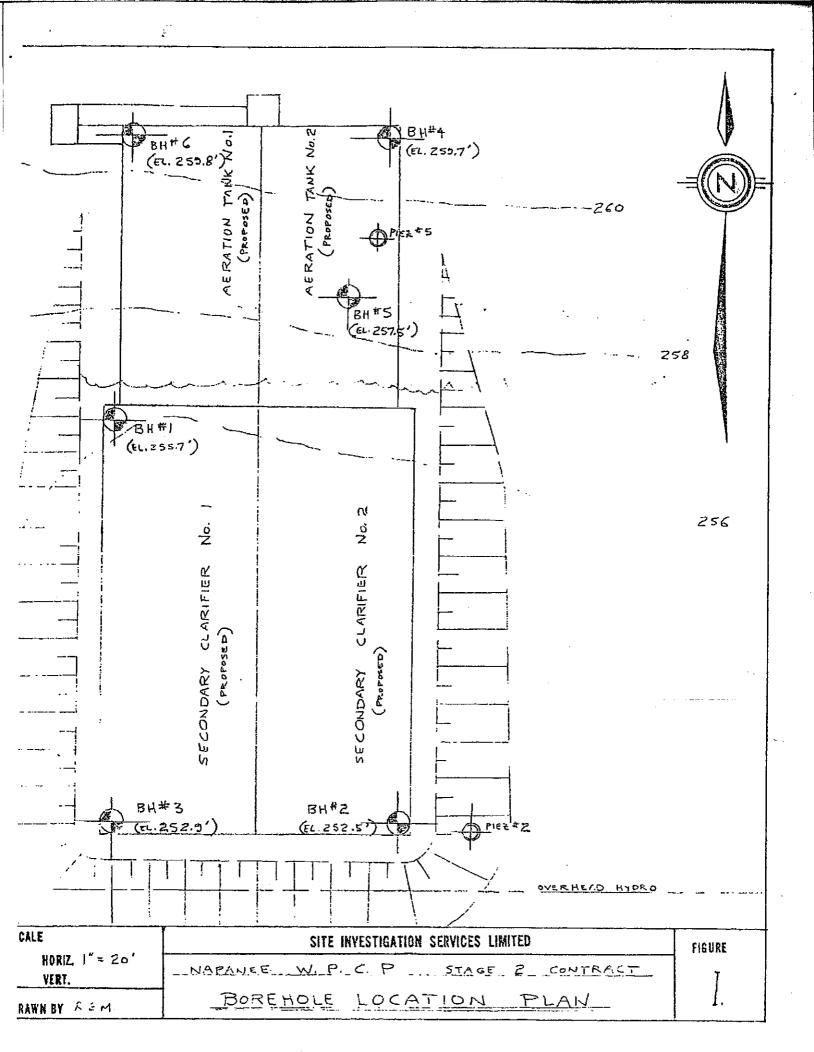
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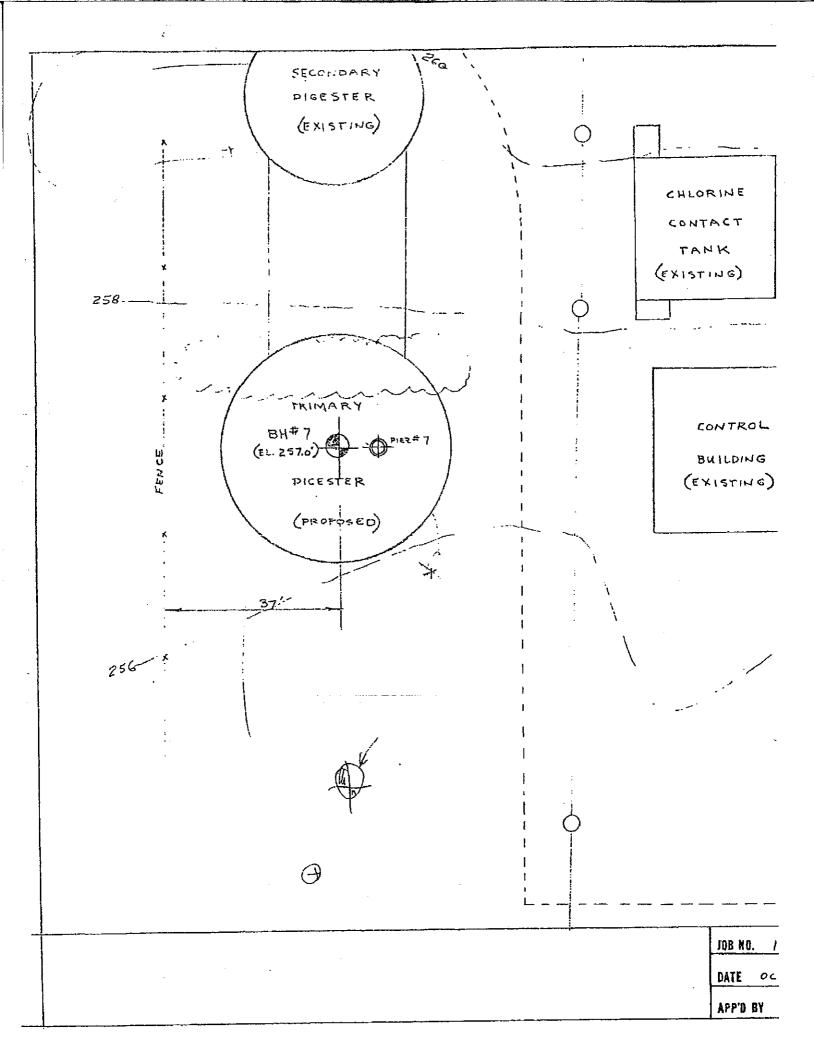
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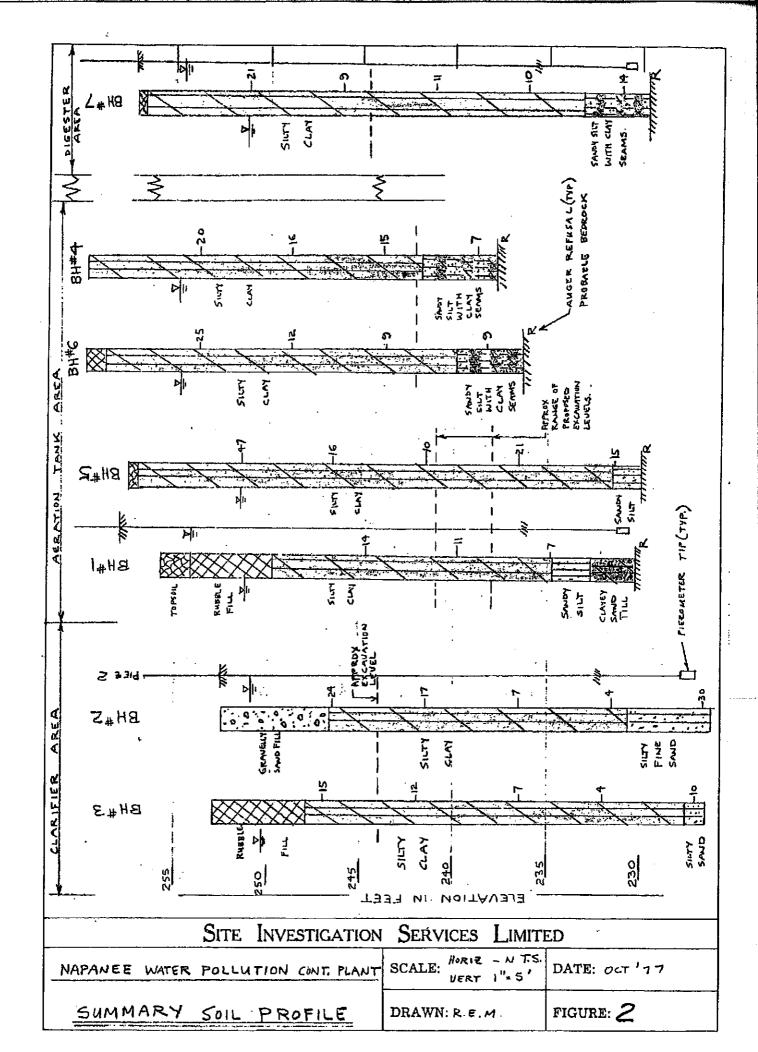
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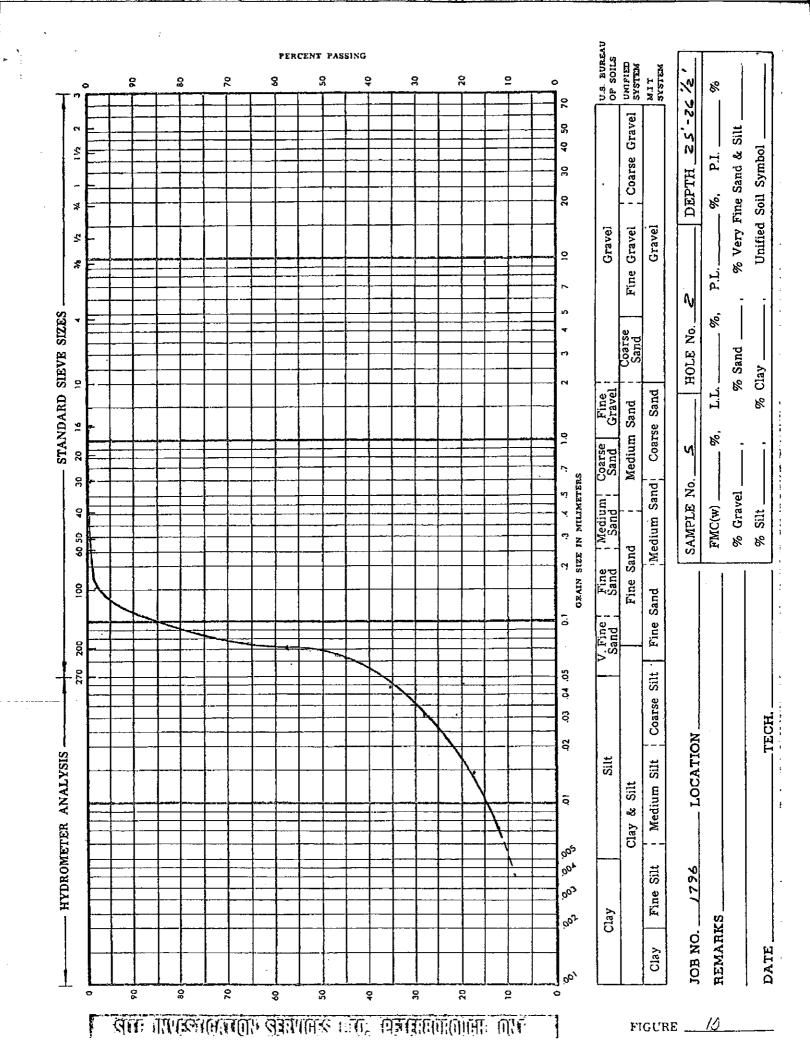
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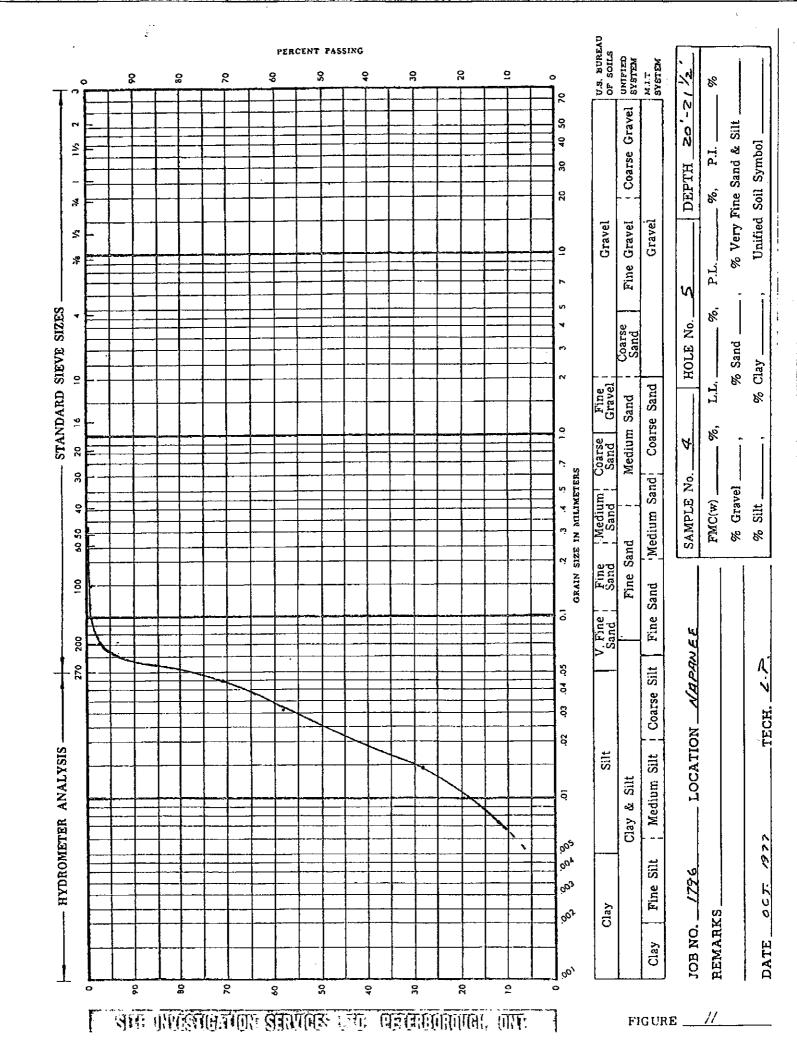
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윈				- H :	SOIL SYMBOL				Language			
SOKEHÇI	NAPANEE W.P.C.P.	STAGE 2			SOIL DESCRIPTION	TOPSOIL SILTY CLAY	-Brown layered silty clay -Some thin sand seams	-Grey below 17 feet			SANDY SILT -Brown sandy coarse silt to silty fine sand	-Some clay seams -Compact NO FURTHER PROGRESS (presumed bedrock)-
ļ	SI	TE 1	NVES	TIGA	TION SE	RVICES Ltd.	JOB No:	1796	BOREHOLE 1	vo: 7	FIGURE No:	9





EXPLANATION OF SYMBOLS AND TEST DATA

SOIL DESCRIPTION

A description of visible characteristics of the soil as determined in the field and altered, if necessary, on the basis of laboratory classification tests.

INORGANIC SOILS









PREDOMINANT
SYMBOL INDICATES
MAJOR SOIL TYPE
EXAMPLE - SILTY CLAY



ORGANIC SOILS











BEDROCK

OTHER SYMBOLS



WATER LEVEL IN BOREHOLE

SAMPLES

Condition:



RELATIVELY UNDISTURBED



DISTURBED



NOT RECOVERED

Type:

D.S. - 1%" ID Drive Sample

A.S. - Auger Sample

U - Thin-walled Tube Sample

UP - Piston Sample

PENETRATION RESISTANCE:

(N) Indicates number of blows, of a 140-lb. hammer falling 30 inches, required to drive a 2" OD Drive Sampler a distance of 1 foot into the soil. This resistance is used to assess the relative density of cohesionless soils and the relative consistency of cohesive soils.

OTHER TESTS

M - Grain size analysis using seives or hydrometer or both - plotted graphically on a separate sheet.

V1 - laboratory vane tests.

Yd - dry unit weight.

C - consolidation test - results on separate sheet.

T - triaxial compression test - results on a separate sheet.

P - proctor compaction test.

K - laboratory permeability test.

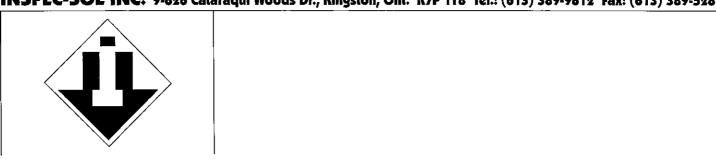
SOILS PROFILES:

Where soil profiles are shown on drawings the soil profile applies only to the borehole location and may be different at intermediate locations on the site.

GROUND WATER:

Ground Water levels are generally measured in the open boreholes and apply to conditions at the time of drilling. Seasonal ground water fluctuations should be expected at most sites.

INSPEC-SOL INC. 9-626 Cataraqui Woods Dr., Kingston, Ont. K7P 1T8 Tel.: (613) 389-9812 Fax: (613) 389-5287



GEOTECHNICAL INVESTIGATION PROPOSED TANK INSTALLATION NAPANEE PLANT – 300 WATER STREET NAPANEE, ONTARIO

NOVEMBER, 1999



Report No. 8131-K6151-A

November 15, 1999

Greater Napanee Water Supply & Pollution Control Board P.O. Box 7
11 Market Square Napanee, Ontario K7R 3L4

Attention: Mr. Al Lucas, Project Manager

RE: Geotechnical Investigation

Proposed Tank Installation

Napanee Plant - 300 Water Street

Napanee, Ontario

Dear Sir:

Inspec-Sol Inc. has completed the fieldwork and engineering for the geotechnical investigation for the above captioned project and we are pleased to submit the following report.

Fieldwork

The scope of work involved the drilling the drilling of two boreholes to 10m or refusal whichever was shallower. The actual depths were approximately 6m where refusal on assumed bedrock was encountered. The logs of the boreholes are attached as Enclosures 1 and 2 and the plan showing the approximate location of the two boreholes is presented as drawing K6151-1

The boreholes were located on the north side of an existing sewage treatment tank and the ground surface had a slope, grading from dropping from north to south. The detailed soil conditions found the boreholes are contained on the attached borehole logs.

Soil and Groundwater Conditions

In summary, the conditions consisted of a fill material that was brown, clay material with pockets of organic staining, gravel sizes and brick fragments. The fill material appeared



to be relatively compact. The fill material was present in borehole BH1 to depths of approximately 4m and only 2m in borehole BH2.

The soils underlying the clay fill consisted of a stiff to very stiff clay which contained seams and/or pockets of silt and sand. In many samples retrieved from the boreholes the silt and sands were very thin but the sample from BH2 at 4.5m there was significant amount of sand retrieved in the sampler.

Refusal was encountered at 5.8 and 5.9m in BH1 and BH2 respectively. It is assumed that refusal is due to bedrock.

The boreholes filled with water during the during the drilling of the borings. The levels were measured on completion or a short time after and were measured at approximately 3 to 3.6m below the ground surface.

The ground surface elevations of the boreholes were measured relative to the top of the rim of the concrete sewage treatment tank. The elevation provided by the clients representative was geodetic elevation 264.0m. The ground surface elevations of the boreholes was then 264.2 and 264.4m for BH1 and BH2 respectively. Based upon this information, the elevation of the measured water levels is 261.2 and 260.8 metres respectively.

Discussions and Conclusions

We understand the client is proposing to install a new treatment tank in the location and will be approximately 4.5m deep. The borehole information suggests that the tank installation will require the removal of fill to reach the native soils. The sides of the excavation will require to be cut back or require shoring. We understand that the contractor selected for this project will be installing a shoring liner system consisting of precast concrete manhole sections and advancing the excavation from within these sections. We understand that the manhole sections will then be part of the permanent tank.

The contractor must be prepared to control groundwater flow as excavations penetrate into the native clay deposit due to wet sand seams. There may also be perched water within the fill soils, especially during wet seasonal periods.

The native soils are considered capable of supporting a bearing pressure of 200kPa(4000psf) for normal spread and strip footings or a mat footing. If higher pressures are required for economical footing design, bearing onto bedrock by spread footings or pile foundations may be an option.



Reference # 8131-K6151-A

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We suggest that this office be retained to review the design concept proposed by the contractor for our comments.

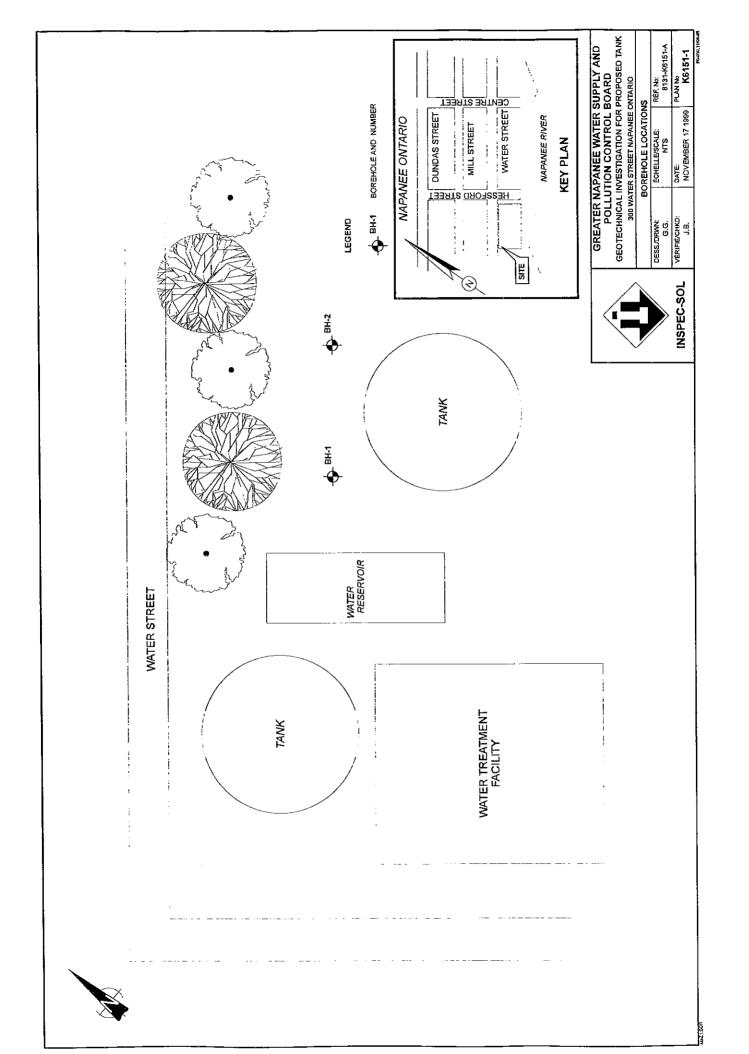
We trust that these comments meet your requirements but should any questions arise please do not hesitate to contact our office.

Yours very truly,

INSPEC-SOL INC.

Jøseph B. Bennett, P. Eng Manager

By fax/mail (613) 354-2836



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	INSPEC-SO	L
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BOREHOLE No.: BH-1
ELEVATION: 258.2m

BOREHOLE REPORT

Page 1 of 1

CLIENT:	TOWN OF NAPANEE	•	LEGEND
PROJECT:	PROPOSED SEWAGE TREATMENT TANK	- 🖂 s	S SPLIT SPOON
LOCATION: _	WATER SEWAGE TREATMENT PLANT, NAPANEE, ONTARIO	_	T SHELBY TUBE
DESCRIBED I	Y: SHANE CASSIDY CHECKED BY: J. BENNETT	BR	C ROCK CORE
			WATER LEVEL

DEPTH	DATE (START)	:	NOVEMBER 5, 1999	DATE (F	INISH):	:	NOVE	MBER 5, 1999		=======================================	-	VVA	NTER	LEV	'EL			
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